

Assessment of aquifer zones and its protection via second-order geoelectric indices in parts of drought-prone region of Deccan Volcanic Province, Maharashtra, India

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Assessment of aquifer protection was studied in the drought-prone regions of Mann Ganga River basin encompassing the districts of Satara, Sangli and Solapur, in Deccan Volcanic Province of Maharashtra, India, using electrical resistivity technique. The study was also aimed at alleviating the drinking water scarcity in these regions. A total of 118 vertical electrical sounding sites were occupied using Schlumberger electrode configuration and the data analysis revealed two to five layered curve types. The modelled layer resistivity and layer thickness at every station were used to calculate the Dar–Zarrouk parameters (i.e., longitudinal conductance S and transverse resistance T). The S values showed that 67% of the area had a poor aquifer protection, whereas 16% had moderate protective capacity and 13% had weak aquifer protective capacity rating. Only 4% of the study area depicted a good protective capacity rating. This indicates that the study area has a rather poor aquifer protective capacity rating, and thereby more prone to infiltrating contaminants. The regions with good-to-moderate protective capacity are envisaged to be potential groundwater zones. The large variation in electrical anisotropy λ ranging from 1 to 2.8 in the study area suggests the anisotropic disposition of the aquifers in basaltic region. The intersection points of several lineaments in the study area are probable to be the most favourable zone for groundwater recharge. This is corroborated by the lineament density of the area, wherein high lineament density reflects high probability of groundwater infiltration. Moreover, the rainfall distribution suggests that the central and eastern parts of the study area receive maximum precipitation, which also coincides with the zones of high lineament density. Particle size analysis was determined from 92 soil samples in the study area and correlated with the longitudinal conductance in order to identify the sub-surface conditions and the aquifer vulnerability. Significant positive correlation was observed between the longitudinal conductance and percentage of clay fraction in the study area. These results could be relied upon for making preliminary estimates of protection from pollution for a sustainable groundwater development and management in future.

Keywords. Electrical resistivity; Mann Ganga River basin; longitudinal conductance; protective capacity; Deccan Volcanic Province.

1. Introduction

Groundwater is a major source for drinking, domestic needs, industrial and agricultural

activities, and thus, its exploration assumes a great implication for the society. However, in today's technologically advanced world, the biggest crisis that human beings facing is water scarcity. This is more severe in the hard rock and drought-prone regions around the globe. This grave situation is due to rising demands of increasing population, over extraction of easily available surface and groundwater resources, increasing human impact on the environment and contamination of available water sources and changing climate, to name a few.

It is a well-established fact that there is relentless scarcity of groundwater in hard rock terrains. The fracturing, faulting, etc. within these hard rock trap limited the amount of groundwater. Some districts of Maharashtra in the hard rock Deccan Volcanic Province (DVP) are no exception to groundwater paucity. However, not much information is available on the lineaments, conduits, joints and fractures in the hydrogeological setup as well as their role in the incidence and movement of groundwater in the semiarid regions of DVP, Maharashtra. Several regions in these districts fall in the rain shadow zone of the Western Ghats. Therefore, an urgent needed for locating the auxiliary sources of groundwater is felt almost all over the region. Hydrogeological mapping can be integrated with geophysical data fruitfully to effectively plan the location of such facilities.

Geophysical investigations are being successfully carried out worldwide for delineating groundwater resources. Electrical resistivity technique is the most popular among all non-invasive geophysical methods due to its relative ease to acquire data, inexpensive instruments, widely available interpretational schemes and relationship between electrical properties, geologic formations and demarcation of aquifers (Zohdy and Jackson 1969; Kotra et al. 2016). To this effect, numerous researchers have extensively used electrical resistivity technique for a variety of problems such as groundwater chemistry of hard rocks (Ramesh and Elango 2012; Mondal *et al.* 2016), saline water intrusion issues (Maiti et al. 2013; Ali Kaya et al. 2015), geothermal explorations (Kumar et al. 2011), environmental assessment (Gómez-Puentes et al. 2016) and geotechnical investigation (Adejumo *et al.* 2015).

The demand for water in the drought-prone regions of Maharashtra has been increasing due to the immense requirement for domestic and agricultural uses, which is further aggravated owing to the paucity of rainfall. Therefore, during the summer months, all the wells go dry and it is seemingly difficult to manage with the existing water supplies. Therefore, to overcome this problem, effective ways of harnessing the groundwater resources are imperative.

During monsoon period, some of the rainwater flows into rivers, lakes and rivulets, whereas some descends into the bowels of the earth's surface due to gravitational effect, passing between soil particles and other rock formation until it reaches the aquifer. However, the rate of groundwater flow depends on the pore spaces and its interconnectivity in the soil. As water percolates through different subsurface layers into the aquifer, it gets filtered: however, there is a thick chance of contaminants being infiltrated beneath. During the course of filtration, the rock matrix acts as sieves, thereby reducing the flow rates as water finds its way through the small pore spaces resulting in long residence time. Vulnerability of an aquifer is related to its ability to resist anthropogenic and natural perturbation, and therefore, it is vital to comprehend the aquifer characteristics. It is reported that residence time of infiltrating water in aquifers with large pore spaces is shorter than that for smaller pore spaces, and consequently, water moves rapidly leading to poor natural filtration process. In such case, it is hard to assuage contaminants by natural filtration. Clay particles overlying an aquifer are protective layers that can offer natural protection to the aquifer from contaminants (Shevnin et al. 2007). The parent rock gets altered into discrete soil particles of varied shapes and sizes due to intense weathering. The disintegrated rocks and weathered regolith materials generally have a wide range of particle size. Soil texture, which is the relative proportions of clay, silt and sand contents, is one of the most vital properties for characterising the soil. The physical and chemical behaviours of soil bear a considerable influence on soil texture with respect to water content and its movement. This parameter not only affects the porosity of soil but also affects soil erosion. Therefore, particle size analysis (PSA) of soils is critical for determining the fitness of soils in terms of protection against contamination and hydrogeological analysis.

Bearing this in mind, proper identification of soil characteristics is also vital as it influences the quality of surface and groundwater, especially in arid and semiarid regions (Engelman and Leroy 1993; Lal and Stewart 1994). Several investigators have applied the combination of electrical resistivity method with water chemistry to decipher the aquifer parameters and quality of water (Mondal *et al.* 2013; Rajesh *et al.* 2015; Batayneh and Al-Taani 2016; and references therein). Few researchers have attempted to evaluate the groundwater potential zones, its contamination and



Figure 1. Geological map of the Mann Ganga River basin in Maharashtra. The VES points and soil sampling locations are also shown.

fertility prospects of soils using PSA and metal contents in soils (Inakwu et al. 2003; Skordas and Kelepertsis 2005; Deshmukh and Aher 2014; Machender et al. 2014). However, very limited literature exists (Delgado-Rodríguez et al. 2011; Islami et al. 2012; Dolui et al. 2016; Kotra et al. 2016), wherein the resistivity data are integrated with physicochemical characteristics of soil with a view to provide information on the subsurface layers and characterisation of the aquifer system and associated vulnerability, if any. The primary objective of the present work is three-fold: (i) to define the aquifer zones within the weathered/fractured basaltic rocks as well as below the traps in the Mann Ganga River basin for groundwater investigation, (ii) to estimate the secondary geophysical indices [Dar–Zarrouk (D–Z) parameters] using vertical electrical sounding (VES) data for assessing the protective capacity of the aquifers and (iii) to establish a qualitative relationship between longitudinal conductance and the soil particle size distribution in the study area. This study, first of its kind in drought-prone region of DVP, Maharashtra, is expected to be a pre-requisite for the delineation of aquifers obscured within and below the Deccan traps and assessment of groundwater potential and its protection ability in the region of interest.

2. Geology and hydrogeology of the study area

The study area is located in the southeastern part of Maharashtra in Satara, Sangli, and Solapur districts. This region, characterised by Mann Ganga River basin, extends from $17^{\circ}00'00''-17^{\circ}50'30''N$ latitudes to $74^{\circ}20'00'' - 75^{\circ}30'00''$ E longitudes. The geological map of the study area is shown in figure 1. The VES and soil sample location points are also marked in figure 1. The total area of the Mann Ganga River basin is 4753.258 km². The maximum elevation of 980 m is observed in the western and northwestern parts of the basin, whereas the minimum elevation is 354 m above mean sea level in the northeastern part. The study area is located on the leeward side of Western Ghats, characterised by the rain shadow zone. The rainfall here is below normal and therefore is a drought-prone region. The average annual rainfall in the Mann Ganga River basin computed during 2001–2015 is about 500 mm.

The entire study area is underlain by Deccan trap basaltic lava flows of upper Cretaceous to lower Eocene age and occupies about 95% of the total study expanse (figure 1). Figure 2 illustrates the general cross-section of hydrogeology in the study area. The flows are represented



Figure 2. General cross-sectional hydro-geological map of the study area.

by compact and massive basalt at bottom and fractured/vesicular portion at top and are separated from each other by thin bole bed. Physiographically, the study area can be broadly divided in four major units, namely (i) hills and Ghats, (ii) foothill zones, (iii) plateaus and (iv) plains. Mann is the major river in the area. The drainage pattern is parallel to semi-dendritic and the drainage density is quite high. The shallow alluvial formation of recent age occurs as narrow stretch along the Mann Ganga River with limited areal extension.

The groundwater occurs under phreatic, unconfined, semi-confined and confined conditions. Generally, the shallower zones down to depth of 20 m below ground level (m bgl) form phreatic aquifer. The water-bearing zones occurring between the depth of 20 and 40 m are weathered and have water under unconfined or semi-confined condition. Deep confined aquifers occur below the depth of 40 m and beyond (CGWB 2013). The fractured and vesicular thickness of different lava flows varies from 8 to 10 m and forms the potential aquifer zones. However, the nature and density of vesicles and their distribution, interconnection, depth of weathering and topography of the area are the important factors for occurrence and movement of groundwater in vesicular unit. It can be seen from figure 1 that almost the entire study area is covered by pahoehoe type flows. This type of flow is reported to be more permeable than the simple type flow (Davis and DeWiest 1966). The massive sections of basaltic lava flows are hard and compact and as such are devoid of primary porosity and permeability; however, the processes of weathering and presence of joints and fractures have developed secondary porosity and permeability (Deolankar 1980).

The yield of dug wells varies between 10 and $190 \text{ m}^3/\text{day}$ in winter season, whereas in summer, it varies between 5 and 20 m³/day. The discharge values of both shallow and deeper aquifer range up to 151 per second as observed from exploration wells in the study area (CGWB 2013). These disparities can be attributed to the hydraulic and morphologic characteristics of the tributaries of

Mann Ganga River. The depth to water level is in the range of 5–20 m bgl in pre-monsoon season, whereas it is about 5–10 m bgl during postmonsoon (CGWB 2013).

3. Survey design and data treatment

A total of 118 VES were carried out within the Mann Ganga River basin (figure 1), adopting Schlumberger electrode configuration with a halfelectrode separation of 100 m, using IGIS (Hyderabad) made SSR-MP-AT resistivity meter. The depth of penetration is proportional to the separation between the current electrodes and provides information on the stratification of the ground (Dahlin 2000).

The preliminary construal of VES data was accomplished using the conventional partial curve matching technique with two-layer master curves in combination with auxiliary point diagrams (Orellana and Mooney 1966). The layer resistivities ρ and thickness h, thus obtained, are served as the initial parameters for computer-aided interpretation using IPI2WIN software, version 3.0.1, a7.01.03 (Bobachev 2003) for interactive semiautomated interpretation. All the sounding curves suggest 2–5 layered structures (see table A1 in the Appendix).

However, there is always an overlapping of resistivity values in certain geomaterials (e.g., clay, water, shale, etc.) (Telford *et al.* 1990; Bhattacharya and Shalivahan 2016), and to minimise the effects of these geophysical similarities in subsurface lithology, secondary geophysical indices, also known as the D–Z parameters (Maillet 1947), are used. The significance of using secondary geophysical parameters is that the contour pattern and boundaries will be distinct, clear and will not display an overlapping character thus reducing the uncertainty in interpretation.

First-order geoelectric parameters (ρ and h) derived were utilised in obtaining D–Z parameters (table A1). The secondary geophysical parameters of significance in this study are longitudinal conductance (S), transverse resistance (T) and electrical anisotropy (λ), which are given by Zohdy *et al.* (1974) for *n*-layer as:

Longitudinal conductance,

$$S = \sum_{i=1}^{n} (h_i / \rho_i), \qquad (1)$$

Transverse resistance,

$$T = \sum_{i=1}^{n} (h_i \rho_i), \qquad (2)$$

where h_i is the saturated thickness of each layer and ρ_i is the true resistivity of each layer.

Coefficient of anisotropy,

$$\lambda = \sqrt{\left(\frac{\rho_t}{\rho_l}\right)},\tag{3}$$

where ρ_t and ρ_l are the average transverse resistivity and average longitudinal resistivity, respectively.

Higher S values generally indicate a relatively thick succession of overburden and is given the highest priority in terms of evaluation of groundwater potential. The S values are also used in evaluating the protective capacity of the aquifer. Henriet (1976) suggested that the earth medium act as a natural filter to the infiltrating fluid and that its ability to hinder fluid is a measure of its protective capacity. Furthermore, the combination of layer resistivity and thickness in the D–Z parameters (S and T) may be of direct use in aquifer protection studies to signify the percolation of contaminants into the aquifer and for the evaluation of hydrologic properties of aquifer (Shailaja *et al.*) 2016). The protective capacity is considered to be proportional to the longitudinal unit conductance (S). Accordingly, the overburden protective capacity was evaluated using the total longitudinal unit conductance (S) values.

Soils samples were collected from 92 sites corresponding to VES locations (figure 1) from 15 to 20 cm depths (the depth of tillage or to the effective rooting depth of plants). Several systems of size classification are used to classify the limits and ranges of soil particle size. In this study, the US Department of Agriculture (USDA) system of classification (Soil Survey Staff 1975) has been used to define the size of the particles. The PSA was evaluated at the Environmental Magnetism Laboratory, IIG, New Panvel.

Soil samples were air dried for several days at room temperature in the laboratory and sieved through 0.25 mm for soil analysis, making sure that no aggregates are retained in the sieve. PSA was performed using a CILAS 1064 laser granulometer with a detection range from 0.03 to 500 μ m. About 200 mg of soil samples was dispersed in sodium



Figure 3. Spatial distribution of longitudinal conductance (S) in the study area.

hexametaphosphate $[Na(PO_3)_6]$ solution and was exposed to ultrasonic treatment for 5 min for a proper disaggregation and dispersion of the soil particles. Later, the ultrasonic-treated soil sample is poured to the sample chamber and laser analysed for the grain size spectrum for a 10-min programme. For data reproducibility, three runs per sample were conducted. Finally, a soil textural triangle was used to determine soil textural class from the percentages of sand, silt and clay in the soil. In the present study, the particle size characteristics of soils are discussed in relation with geophysical indices (longitudinal conductance S) and their effect on protective capacity of aquifers. Depending on the size distribution, primary particles (< 2 mm) are usually divided into three classes, e.g., sand, silt and clay.

4. Results and discussion

4.1 Estimation of D-Z and other parameters

As stated earlier, a total of 118 VES were carried out via Schlumberger configuration in the drought-prone, hard-rock terrain of DVP encompassing Mann–Sangola–Jath–Atpadi subdivisions of Satara, Solapur and Sangli districts of Maharashtra (figure 1). The D–Z parameters were calculated to estimate the protective capacity of the underlying aquifers from infiltrating contaminants, which will provide a perception of the spatial variation of these parameters to demarcate the fresh water bodies and to delineate the groundwater potential zones.

The longitudinal conductance (S) value estimated from equation (1) varies from a minimum of 0.0023 S to a maximum of 1.605 S (figure 3). The spatial variation map further depicts that the eastern, southern and northwestern parts are infested with low S values (0.0023–0.05 S). The central and western parts are characterised by relatively high S values greater than 0.1 S.

According to Oladapo and Akintorinwa (2007), clayey overburden is characterised by reasonably high longitudinal conductance and offers protection to the underlying aquifer from contaminants to permeate. The modified classification of aquifer protective capacity rating (Oladapo *et al.* 2004) facilitates to categorise an area into poor, weak, moderate, good, very good and excellent protective capacity zones (table 1).

The longitudinal conductance map (figure 3) suggests that the protective capacity rating over the entire basin is about 67%, which is rather poor. About 4% of the area falls within the good

protective capacity, whereas about 16% represents moderate protective capacity rating and the remaining 13% exhibits weak protective capacity. This implies the fact that major part of the study area, which is characterised by relatively poor-toweak capacity rating, is more prone to percolating contaminants. These results further suggest that the areas with moderate-to-good aquifer protective capacity correspond with zones of significant clayey overburden, which are sufficient enough to protect the aquifer from contamination.

The total transverse resistance (T) calculated from equation (2) varies from 106 to 104,951 $\Omega \,\mathrm{m}^2$ in the study area (figure 4). It is quite evident that high T values (>4000 $\Omega \,\mathrm{m}^2$) represent the fresh water regime. The parts of central, eastern,

Table	1.	Modif	ied	pr	otective	capacity	rating
(after	Ol	adapo	et	al.	2004).		

Longitudinal conductance (S)	Protective capacity rating
>10	Excellent
5-10	Very good
0.7 - 4.9	Good
0.2 - 0.69	Moderate
0.1 - 0.19	Weak
< 0.1	Poor

southern and northwestern sectors of the study area (figure 4) signify fresh water zones. These areas are also depicted with low S values. Higher Tvalues usually reflect high transmissivity and thus, highly porous to fluid movement. Hence, there is a possibility of enhanced passage of contaminants into the groundwater (Tsepav *et al.* 2015). The southwestern and central parts of the study area are characterised by low T values (<4000 Ω m²).

The resistivity of a layer depends more on the saturation of the layers and not necessarily on the thickness of the aquifer; hence, higher resistivity may not correlate with areas with thicker aquifer. Aquifer resistivity varies from 10 to 9385 Ω m in the study area (figure 5). The central part and the pockets of western sector of the study area are characterised by low aquifer resistivity values (10–60 Ω m), signifying that it has a good groundwater potential. However, the northern, northeastern and southern parts divulge high values of aquifer resistivity.

The highly thick aquifers possess higher groundwater potential. The variation in aquifer thickness in this region (figure 6) can be ascribed to topography and geological structure. The aquifer thickness values vary from a minimum of 0.336 m to a maximum of 75.7 m. The spatial variation of aquifer thickness suggests that the western part,



Figure 4. Spatial distribution of transverse resistance (T) in the study area.



Figure 5. Spatial distribution of aquifer resistivity in the study area.



Figure 6. Spatial distribution of aquifer thickness in the study area.

surrounded by the foothills of Western Ghats, is having a thickness ranging from 25 to $70 \,\mathrm{m}$. Similarly, stretches of northern and eastern parts reveal aquifer zones with thickness varying from 30 to 60 m. It may be mentioned here that the northeastern part of the study area is underlain by Sangola



Figure 7. Spatial distribution of electrical anisotropy (λ) in the study area.

high as advocated by several researchers (Tiwari *et al.* 2001; Pandey *et al.* 2009), to be discussed later.

The average longitudinal resistivity ρ_l ranges from 11.5 to 3327 Ω m in the study area, which helps in calculating the total depth H to the high resistivity bedrock. This wide variation in resistivity values also reveals the degree of subsurface inhomogeneity (Murali and Patangay 2006). Furthermore, the average transverse resistivity ρ_t varies from 13.4 to 5045 Ω m, which is more than the average longitudinal resistivity (Salem 1999). This indicates that the current flow and average hydraulic conduction along the lithology boundary are greater than those normal to the boundary plane (Ndatuwong and Yaday 2015).

Based on the estimates of transverse and longitudinal resistivities, the coefficient of electrical anisotropy λ is calculated using equation (3). This is a measure of the extent of inhomogeneity in the basement caused due to the near surface effects, extent of weathering and geological features such as fractures, lineaments, faults, etc. (Ayuk *et al.* 2013). The value of λ ranges from 1 to 2.8 with an average of 1.24 in the study area and its distribution is shown in figure 7.

This dimensionless parameter generally varies between 1 and 2 in most of the geological environments (Zohdy *et al.* 1974). Keller and Frischknecht (1966) are of the view that λ increases with the hardness and compaction of rocks, and therefore, such areas can be related with low porosity and permeability. This parameter is generally used to evaluate the fitness of the underlying geomaterials and identify the locales of potential aquifer zones with high porosity and permeability. Singh and Singh (1970) advocated that an area with λ value ranging between 1 and 1.5 is considered to be a potential zone for groundwater.

It can be observed from figure 7 that the coefficient of anisotropy suggests an increasing trend from southwest (SW) to northeast (NE) direction with λ values >1.6. Similar increasing trend is also observed in the northwest (NW)– southeast (SE) direction. This reveals the heterogeneous and anisotropic nature of the subsurface in both NE–SW and NW–SE directions. These stretches are, thus, more fractured in the study area, suggesting reasonably enhanced prospective groundwater zone (Mondal *et al.* 2013).

For a better understanding of the subsurface features, the lineaments (redrawn after http:// bhuvan.nrsc.gov.in/state/MH) have been superimposed on the electrical anisotropy map (figure 7) that also depicts the course of Mann Ganga River. This river originates near Mann village (VES 68 and 69) and flows in SE direction until it takes a sharp turn (near VES 78 and 77) and changes its course towards NE direction. It can be seen from the figure 7 that two major lineaments trending NE–SW and NW–SE directions near Sangola is parallel to the course of Mann Ganga River, which is the causative factor for the river to take a sharp turn. Geophysical studies (Krishna Brahmam and Negi 1973: Tiwari et al. 2001: Pandev et al. 2009: Vasanthi and Satish Kumar 2016) have delineated a WNW-ESE trending gravity high around Sangola, which has been attributed to the upliftment of lower crust and uppermost mantle. This suggests that high-density material is underlying beneath this region. Furthermore, Krishna Brahmam and Negi (1973), from residual gravity anomalies, are of the view that the Sangola high is flanked by gravity lows at Karad and Kurduwadi, and the distinct gravity high is due to tectonic activity, indicating displacements in deeper strata. The spatial variation of electrical anisotropy (figure 7) reveals high λ values near Sangola, marked by lineaments extending in all directions, which might be the surface expression of Sangola high. These have better water-holding capacity from different directions. Furthermore, figure 7 reveals several lineaments criss-crossing the study area, and the intersection points of these lineaments are probably to be the most favourable zone for groundwater recharge.

As mentioned earlier, the electrical anisotropy λ ranges from 1 to 2.8, depicting a broad variation in the study area, suggesting the nature of anisotropy of the geoelectrical parameters. It has been reported by Kumar *et al.* (2014) that if λ exceeds 1, then the subsurface basaltic formation is more fractured; on the other hand, if the value of λ is about 1, then probably the overburden thickness *H* is more. In the present study, the maps of electrical anisotropy and aquifer zone thickness suggest that the VES stations with relatively thick overburden are hovering around the λ value of 1. This also reveals that the lineaments are more conspicuous at places with high λ values, as can be observed in figure 7.

Lineaments are the surface expression of the underlying geological structure such as fault. Lineament density map is essentially used to assess the relationship between lineaments and groundwater occurrence. The lineament map was generated from the satellite image, toposheets and field inspection of the study area. The lineament density (L_d) is the fraction of total lineament length divided by the total area of the basin (Edet *et al.* 1994). The mathematical expression of lineament density is as follows:

Lineament density,
$$L_d = \sum_{i=1}^n \left(\frac{L_i}{A}\right)$$
.

where A (in km²) is an area of grid and $\sum L_i$ is total lineament length (in km) in the area under consideration. In the study area, the lineament density ranges from 0 to 2.18 km/km² (figure 8). High lineament density values generally suggest high-yielding borewells. Therefore, the high lineament density (1.24–2.18 km/km²) in the central and north western parts of the study area implies high possibilities of groundwater percolation and vice versa.

Rainfall is one of the key parameters which is directly related to the groundwater potential of an area. It determines the amount of water percolated into the subsurface. Rainfall data were obtained from Tropical Rainfall Measuring Mission (TRMM) database and combined with IMD data. The tiled TRMM data were again reclassified to match pixel data size of other layers. Pixel data values were extracted to point layer for preparation of rainfall map of the study area (figure 9). The maximum rainfall (710–1046 mm/yr) is concentrated in the central and eastern parts of the study area.

4.2 Interrelationship between thematic parameters

As mentioned earlier, the present study area Mann River basin is underlain by DVP, and groundwater occurs in unconfined and semi-confined conditions. The major rock type in this area is the basaltic rock unit that do not have any primary porosity, and thus, the occurrence and movement of groundwater are possible through the secondary porosity, which is developed due to weathering and fracturing (Deolankar 1980). Groundwater occurrences are mainly concentrated to shallow overburden of weathered materials and fractured bed rocks. In view of this, the main focus of the present study is to locate unconfined aquifers up to depths of 40 m, although deeper confined aquifers at depth of 60 m and more are also evident at some VES stations.

From the above, it can be inferred that the central and western parts of the study area depict low aquifer resistivity values and moderate aquifer thickness, suggesting that these regions are favourable for groundwater. Moreover, the longitudinal conductance (S) map reveals that these parts of the study area have moderate-to-good



Figure 8. Lineament density (L_d) map of study area.



Figure 9. Rainfall distribution map of the study area.

protective capacity, implying that the overburden clayey layer is considerably thick and offers protection to the underlying aquifers from contaminants. The transverse resistance (T) divulge low values in the central and western parts of the study area, meaning that the transmissivity is low and infiltration of contaminants will be minimum.

It can be deduced from the foregoing that high groundwater potential zones are predominant in the central part of the basin showing low-tomoderate aquifer resistivity and high lineament density. The parallel between electrical anisotropy and lineament density maps (figures 7 and 8) also reveals that regions with high lineament density coincide with the heterogeneity of the subsurface. These stretches, therefore, tend to be more prolific, owing to the openings that exist in the form of joints and fractures that allow groundwater to move easily. Similarly, it is seen from figures 8 and 9 that the regions near Mhaswad and Sangola having highest rainfall are demarcated with high lineament density, which is an indicative of high groundwater recharge zones.

4.3 Relationship between longitudinal conductance and soil fraction

The soils of the study area are primarily derived from the Deccan basalt (Deshpande 1998). This region has distinctive landform wherein, the western and northwestern parts are prevalent with structural and denudational hills, whereas the central and eastern portions are characterised by plain area. As this area has a typical climatic condition characterised by meagre rainfall, severe drought is prevalent, distinctive of a semiarid environment. Therefore, the soils will be more fragile and prone to degradation. On the whole, the soil from the study area shows the presence of both nodular as well as powdery calcrete, assortment of clay, sand and silt besides the fragments of weathered basalt (Duraiswami *et al.* 2012). As mentioned earlier, the study region falls in the rain shadow zone, and thus, there is severe scarcity of water. The problem of water scarcity and contamination is also aggravated due to over irrigation, excessive use of chemical fertilisers and intensive rainless crops cultivation.

The PSA data suggest that silt is dominating the entire basin, followed by sand and finally by clayey type of soil. The clay content varies from a minimum of 5.55% to a maximum of 32.78%. The silt content varies from 47.47 to 89.55%, whereas the

sand content ranges from 0 to 45.42%. As stated earlier, the aquifer protective capacity in the study area is poor (67%). This is further established by the fact that the clayey overburden is not thick enough over the entire basin, thereby enhancing the infiltration of contaminants.

As discussed earlier, highly impervious materials such as clay usually have high longitudinal conductance S values, thereby offering good protection to the underlying aguifers, whereas sand have low longitudinal conductance values that are associated with low aquifer protective capacity. The downstream part of the Mann River and its tributaries to the southern side is dominated by silt which is usually more fertile than other types of soils and is useful for agricultural purposes. The spatial distribution of clay in the study area (figure 10) is spread over the entire basin in patches. A look at the spatial distribution of clay and longitudinal conductance map (figure 3) reveals that regions with moderate to high S values are reflected with clayey layer varying from 15% to 32%. Clay particles are very important in soil fertility as they have high water holding capacity and poor percolation. The sand particles are pervasive in the upstream part of Mann River. In the downstream part, however, it is negligible due to plain topography characterised by alluvial lithology.

It has been reported by Deshmukh and Aher (2014) that particle size distribution influences the moisture retention and transmission properties of soils. This means that coarse textured soils (sand) have low moisture retention and high permeability, whereas fine textured soils (clay) have high moisture retention and low permeability. In the present study area, it can be surmised that regions where soils have high clay content, the contaminated water will have extended travel time to percolate from the surface to the low permeability aquifers, thereby protecting the deep aquifers from pathogen contamination. The clay portion contains larger aluminosilicates and has higher content of humus. Moreover, the electrical resistivity is connected to the particle size by the electrical charge density at the surface. Clay minerals have a high cation exchange capacity, and because of their proportion in weathered crystalline rock terrains, they yield a low electrical resistivity. This is due to the effect of conduction mechanism located in the close vicinity of pore water-mineral interface in the electrical double-layer coating the mineral-water interface (Revil and Leroy 2001). The electrical double-layer contributes to the enhancement of



Figure 10. Spatial distribution of clay in the study area.

the electrochemical properties of the clay minerals (Leroy and Revil 2004). In clayey soil, the electrical charges located at the surface of the clay particles lead to lower electrical resistivity than in coarse-textured soils because of the magnitude of the specific surface (Fukue *et al.* 1999).

5. Conclusions

In this study, geoelectrical sounding data have been used to study the aquifer protective capacity and delineating aquiferous zones utilising the secondary geophysical parameters (D–Z parameters) and other thematic parameters in the drought-prone region of southern Maharashtra.

The longitudinal conductance S value varies from a maximum of 1.605 S to a minimum of 0.0023 S in the study area. The S map further reveals that about 80% of the study area is characterised by topsoil with poor-to-weak protective capacity. This implies that alluvium aquifers in the basin are not protected against infiltrating contaminants. This has helped to assess the shallow subsurface materials overlying the aquifers in the study area, thereby enabling the evaluation of the vulnerability of aquifers to surface pollutants such as chemical fertilisers that are commonly used by farmers in the rain-shadow region of the Mann Ganga River basin.

The total transverse resistance T varies from 106 to 1,04,951 Ω m². High T values in excess of 4000 Ω m² in central, eastern, southern and northwestern parts of the study area signify fresh water regime. This also reflects high transmissivity and hence highly permeable to fluid movement.

The coefficient of anisotropy divulge an increasing trend from SW–NE and NW–SE directions with λ values >1.6, revealing the heterogeneous and anisotropic disposition of the subsurface in these directions. These stretches are, both therefore, more fractured suggestive of enhanced potential groundwater zone. Furthermore, several lineaments are traversing throughout the study area, and the intersection points of these lineaments are expected to be the most favourable for groundwater recharge in the area. The lineament density map also corroborate with the heterogeneity of the subsurface. It is also inferred that the central region is characterised by highest rainfall where high lineament density is revealed. These areas are suggestive of high groundwater recharge zones.

The PSA data suggest that silt is dominating the entire basin, followed by sand and clay types of soil. The spatial distribution of clay and longitudinal conductance (S) map suggests that regions with moderate to high S values are observed, where the clay overburden is relatively thick.

The estimation of D–Z parameters for appraisal of aquifer protection studies is of utmost significance in terms of societal issues such as groundwater exploration and protection from pollution. Furthermore, this result will be useful to achieve a better perceptive of the complex geology of the Mann Ganga River basin and should provide basis for the assessment of large tracts of drought-prone agricultural land using electrical resistivity imaging and VLF-EM to achieve sustainable groundwater management, hydrologic and hydrogeologic evaluations.

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Appendix

Table A1. Geoelectrical layers and D-Z parameters in the Mann Ganga River basin, Maharashtra.

VES		Laye	r resist	tivity (Ω	m)		I	layer th	icknes	s (m)							
no.	ρ_1	ρ_2	$ ho_3$	$ ho_4$	$ ho_5$	ρ_6	h_1	h_2	h_3	h_4	h_5	$H(\mathbf{m})$	S	T	λ	$ ho_t$	$ ho_l$
1	61.5	191	129	27.4	111		0.5	1.93	13.5	7.1		23	0.382	2335	1.29	101	60
2	30.4	97.4	80.8				0.5	11.8				12.3	0.137	1164	1.02	94.6	89.7
3	31.5	96.4	79.3				0.5	13.8				14.3	0.159	1346	1.02	94.1	89.9
4	37.5	2024	234	44	35.4		0.5	0.187	27	8.89		36.6	0.33	7106	1.32	194.1	110.9
5	36.5	80.2	36.2	91.3			0.5	2.65	8.33			11.5	0.27	532.3	1.04	46.2	42.5
6	67.3	125	73.8	193			1.03	3.3	55.9			60.2	0.799	4607	1	76.5	75.3
7	263	17.5	219				0.71	0.336				1.05	0.021	192	1.9	183	50
8	48.5	136	62.7	163			1	9.23	34.5			44.8	0.638	3466.9	1.04	77.3	70.2
9	16.1	134	55.9	105			1.32	3.19	18.8			23.3	0.43	1499	1.09	64.3	54.1
10	41	106	98				0.5	25				25.5	0.248	2670	1.01	104.7	102
11	59.9	198	135	89.5			0.557	2.96	21.9			25.4	0.186	3575	1.01	140.7	136
12	20.8	189	82.8				2.22	10.6				12.8	0.162	2049	1.42	160	79
13	120	90.3	116				0.613	2.17				2.78	0.029	269.5	1	96.9	95
14	35.3	226	61.3				0.565	8.14				8.71	0.05	1859	1.1	213.4	174.2
15	47.6	101	668	103			0.738	6.75	3.03			10.5	0.086	2740	1.46	261	122
16	55.8	107	75.7				0.5	3.2				3.7	0.038	370.3	1.01	100	97.3
17	107	282	70.3				2.94	19.8				22.8	0.097	5898	1.04	258.6	235
18	119	32.6	410	26.9	4430		2.13	1.046	3.37	35.3		42.2	1.38	2632	1.42	62.3	30.5
19	49	206	106				0.5	0.934				1.43	0.014	216.9	1.21	151	102
20	24.7	37.3	125				0.5	6.21				6.71	0.186	243.9	1	363	36
21	34.3	155	897	42.5			0.587	3.86	2.94			7.38	0.045	3255	1.63	441	164
22	189	415	95.8				0.556	0.628				1.18	0.0044	365	1.07	309.9	268
23	108	203	46.7				1.8	16.9				18.7	0.099	3625	1.01	193.8	188
24	43.5	503	105				0.5	0.329				0.829	0.012	187	1.8	225	69
25	60.6	680	162	90.9			0.5	0.274	8.2			8.97	0.059	1545	1.06	172	152
26	104	225	17.7	1487			0.659	6.39	27.8			34.8	1.605	1998	1.6	57.4	21.6
27	89.5	132	108	278	64.2		0.5	2.14	12	6.49		21.2	0.156	3427	1.09	161	135
28	58.1	149	72.4				0.669	21.3				22	0.154	3212	1.01	146	142
29	46	123	50	113			0.5	2.88	17.6			21	0.386	1257.2	1.04	59.8	54.4
30	61.4	84.4	235	107			0.5	5.54	12.2			18.2	0.125	3365	1.12	184	145
31	50.1	166	10.2	19190			1.38	3.14	7.37			11.9	0.769	665	1.9	55.9	15.4
32	33.7	176	84.1				0.515	14.6				15.1	0.098	2586	1.01	171	167.7

Table A1. (Continued.)

VES		Lay	er resis	stivity (Ω	2m)]	Layer ti	hicknes	s (m)							
no.	ρ_1	ρ_2	$ ho_3$	ρ_4	ρ_5	ρ_6	h_1	h_2	h_3	h_4	h_5	$H(\mathbf{m})$	S	T	λ	ρ_t	$ ho_l$
33	59.8	208	146	75.2			0.5	2.26	15.6			18.3	0.126	2777	1.02	151.7	145
34	34.7	94.3	70.7				0.506	20.4				20.9	0.23	1941	1.01	92.8	90
35	45.3	208	75.8				1.22	2.79				4.01	0.04	635.5	1.25	158	100
36	58.5	83.7	169	62.8			0.5	5.81	20.7			27	0.2	4013.8	1.04	148	135
37	53.9	157	79.9				0.596	9.81				10.4	0.073	1572.2	1.03	151.1	142
38	43.4	155	33.5	67.6			0.609	2.74	6.57			9.92	0.227	671.2	1.24	67.6	43.7
39	42.2	903	0.861				0.5	7.28				7.78	0.019	6594	1.43	847	409
40	18.5	84.8	47				6.02	0.553				6.58	0.331	158.2	1.12	24	19
41	5.16	15.1	64.7				1.25	6.64				7.88	0.68	106	1.08	13.4	11.5
42	37.5	117	198	59.2			0.5	3.54	8.21			12.3	0.085	2058	1.07	167	144
43	90.3	365	86.0	597	54.6		0.644	0.628	3.72	3.33		8.32	0.057	2595	1.46	311.9	145
44	23.6	121	77.8				0.911	19.2				20.1	0.197	2344	1.06	116	102
45	103	164	43.7	114			0.677	5.18	25			30.8	0.61	2011	1.14	65	50
46	59.9	196	54				0.573	13.1				13.7	0.076	2601	1.02	189.9	180
47	80.9	107	74.6	52.9			0.73	2.45	20.5			23.7	0.306	1850	1	78	77
48	52	96.7	18.1	107			1.14	14.9	6.62			22.7	0.54	1619	1.3	71.3	42
49	230	1401	275	2277	503		0.5	0.836	2.23	22.4		26	0.99	2409	1.8	92.6	26
50	4270	656	139	126582			0.774	4.27	9.28			14.3	0.073	7396	1.62	517	195
51	966	9379	1797	404			1.38	2.95	15.5			19.8	0.01	56854	1.2	2871	1980
52	309	2067	21.9				1.84	43.2				45	0.026	89862	1.07	1996	1730
53	418	1142	560				0.581	6.55				7.13	0.0071	7722	1.03	1083	1004
54	1320	433	6768	721			3.92	2.94	7.68			14.5	0.01	58425	1.6	4029	1450
55	1901	1201	5206	678			2.3	5.35	4.48			12.1	0.0065	34120	1.24	2879	1861
56	412	5475	325	5598	25.3		0.5	0.524	1.7	18.1		20.8	0.0097	104951	1.53	5 045	2144
57	532	2157	78.7	789	-0.0		0.923	2.87	5.89	1011		9.68	0.077	7145	2.42	738	125
58	109	1569	427				0.529	8.85	0.00			9.38	0.01	13943	1.25	1486	938
59	190	1333	12.7				4.1	30.2				34.3	0.044	41035	1.23	1196	779
60	149	1140	6030	141			0.513	9 79	11 1			21.4	0.013	78170	1 48	3652	1646
61	1673	376	1900	666			0.944	0.583	10.9			12.5	0.010	22508	1.10	1800	1602
62	1077	2617	253	549			0.876	2.95	8.53			12.4	0.035	10821	1.56	872.6	354
63	369	1450	1017	0 10			0.649	2.28	0.00			2.93	0.0033	3545	1 16	1210	887
64	2230	653	2418	463			0.522	0.393	14 7			15.6	0.0069	36965	1.02	2369	2260
65	886	3249	346	835			1.86	2.9	12.1			16.9	0.037	15256	1.14	<u>-</u> 000	456
66	2600	965	653	000			0.746	$\frac{2.0}{4.07}$	12.1			4 82	0.001	5867	1.06	1217	1071
67	975	1489	1008				0.5	3.07				3.57	0.00257	5058 7	1.00	1417	1389
68	3391	650	1675	221	1584		0.5	2 29	10.6	10.2		23.6	0.056	23193	1.52	982	421
69	3699	1683	203	833	1001		0.5	3.1	3 64	10.2		20.0 7 24	0.019	7805	1.68	1078	381
70	1205	344	200 447	1185			0.5	0.836	8.2			9.53	0.021	4555	1.02	478	453
71	524	4544	669	2197	832		0.5	0.129	6.04	7.2		13.9	0.013	20707	1.18	1489	1069
72	713	7768	147	2531	418	1062	0.5	0.233	0.644	1.97	21.8	25.1	0.052	6359	1.16	651.7	482
73	1124	4205	455	2001	110	100-	1.89	174	01011	1.01		19.3	0.0058	75291	1.08	3901	3327
74	478	1079	455				0.5	24.1				24.6	0.0233	26242	1	1066	1055
75	392	130	1589	650			0.714	4 56	14.6			19.9	0.0260	24072	1 67	1209	432
76	1230	912	564	000			0.5	6.86	11.0			7 36	0.0079	6871	1	933	931
77	608	1082	4248	164			0.906	18.6	10			29.6	0.0015	63156	1 23	2133	1409
78	90 Q	38.6	803	104			0.500	5	10			5 5	0.021 0.135	238 /	1.20	2100 /3 3	1405
79	1443	973	500				0.5	197				20.2	0.100	19889	1	984.6	981
80	866	3100	381	929			3.11	5.63	12.9			21.6	0.039	25061	1.44	1160	553.8
81	1213	2666	869	168			3 91	1.51	28.5			33.9	0.036	33534	1.02	989	941
82	46.6	20.3	39.8	2774			0.5	0.928	<u>20.0</u> 8 11			9 54	0.26	364	1.02	38.2	36
83	193	51.5	163	2111			0.636	1.52	0.11			2.16	0.032	201	1 17	93	67.5
84	790	309	1179				2.21	3.86				6.07	0.015	2938	1 00	484	404
85	216	443	204	1301			0.68	2.83	6 69			10.2	0.042	2765	1.05	271	242
55		110	-01	1001			0.00	2.00	0.00			10.4	0.014	00	1.00	- · ·	- 14

VES		Laye	r resisti	2m)		L	ayer th	icknes	s (m)								
no.	ρ_1	ρ_2	$ ho_3$	$ ho_4$	$ ho_5$	ρ_6	h_1	h_2	h_3	h_4	h_5	$H(\mathbf{m})$	S	T	λ	$ ho_t$	$ ho_l$
86	237	2896	1185				0.524	0.507				1.03	0.0023	1592	1.88	1546	434
87	1242	774	1913	582			0.5	3.26	4.7			8.46	0.007	12135	1.08	1434	1208
88	395	619	693				0.5	14.4				14.9	0.0245	9111	1	611.4	608
89	180	71.3	394				3.46	6.26				9.72	0.107	1069	1.1	109.9	908
90	765	1082	344	870			0.5	8.81	14.5			23.8	0.05	14902	1.14	626	476
91	116	185	31.7	318			0.883	3.46	4.69			9.03	0.041	2229	1.05	246	220
92	133	23.6	32816				0.635	2.38				3.02	0.1	140.6	1.24	46.5	30.2
93	101	400	1398	335			0.731	13.3	19.8			33.9	0.054	33074	1.24	975	627
94	648	287	980				1.4	8.02				9.42	0.03	3208	1.04	340	314
95	219	438	7483	585			0.554	2.31	2.02			4.88	0.008	16248	2.3	3329	610
96	572	802	1338	84.6			0.5	3.47	75.7			79.7	0.061	104355	1.04	1309	1207
97	98.2	1808	269	2032			0.5	3.08	596			9.54	0.028	7220	1.049	756	340
98	86.2	33.1	716				0.787	4.75				5.54	0.152	225	1.06	40.6	36
99	843	14028	1285	3768	147	1087	0.5	0.125	2.8	4.71	2.9	11	0.023	23946	2.19	2176	478
100	2406	814	1373				0.511	4.44				4.95	0.0056	4843	1.1	978	883
101	1566	362	876				0.583	14.2				14.8	0.039	6053	1.03	409	379
102	1224	33.6	260	2271	11.5		0.5	0.156	7.59	29.8		38	0.047	70266	1.5	1849	808
103	1159	2033	225	4032			3.57	5.96	59.5			69	0.27	29641	1.29	429	255
104	821	5612	1356	836			2.58	1.44	38.9			43	0.032	62947	1.09	1618	1343
105	975	258	9385	1152			2.53	1.54	1.85			5.91	0.008	20226	2.15	3422	738
106	40	22.5	526				1.32	10.8				12.1	0.513	295	1.02	24.4	23
107	807	1526	3301	862			0.5	3.38	6.25			10.1	0.004	26192	1.01	2593	2525
108	257	177	6287	237			1.17	524	10.4			16.8	0.035	66612	2.8	3965	480
109	137	80.6	652				0.5	2.05				2.55	0.029	233	1.02	91.6	87
110	220	1320	62.5				1.38	62.6				64	0.053	82935	1.03	1295	1207
111	557	124	1036	41.5			0.551	0.741	64.7			66	0.069	67427	1.03	1021	956
112	68.1	373	939				0.5	7				7.5	0.046	2645	1.46	325.6	163
113	327	981	6050	608			1.33	9.48	6.03			16.8	0.014	46216	1.51	2750	1200
114	936	431	372	551			0.5	3.25	51.1			54.9	0.14	20877	1	380	378
115	109	16.5	113	670			0.626	0.571	5.65			6.85	0.09	716	1.16	104	76
116	24.7	37.3	125				0.5	6.21				6.71	0.186	243	1	36.3	36
117	704	3291	796	5682			0.541	0.236	63.7			64.5	0.087	51093	1.03	792	741
118	436	2043	641				1.07	19				20.1	0.011	39283	1.03	1954	1827

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